

Frequency- and Time- Domain Methods of Defect Detection in Water Pipeline Systems

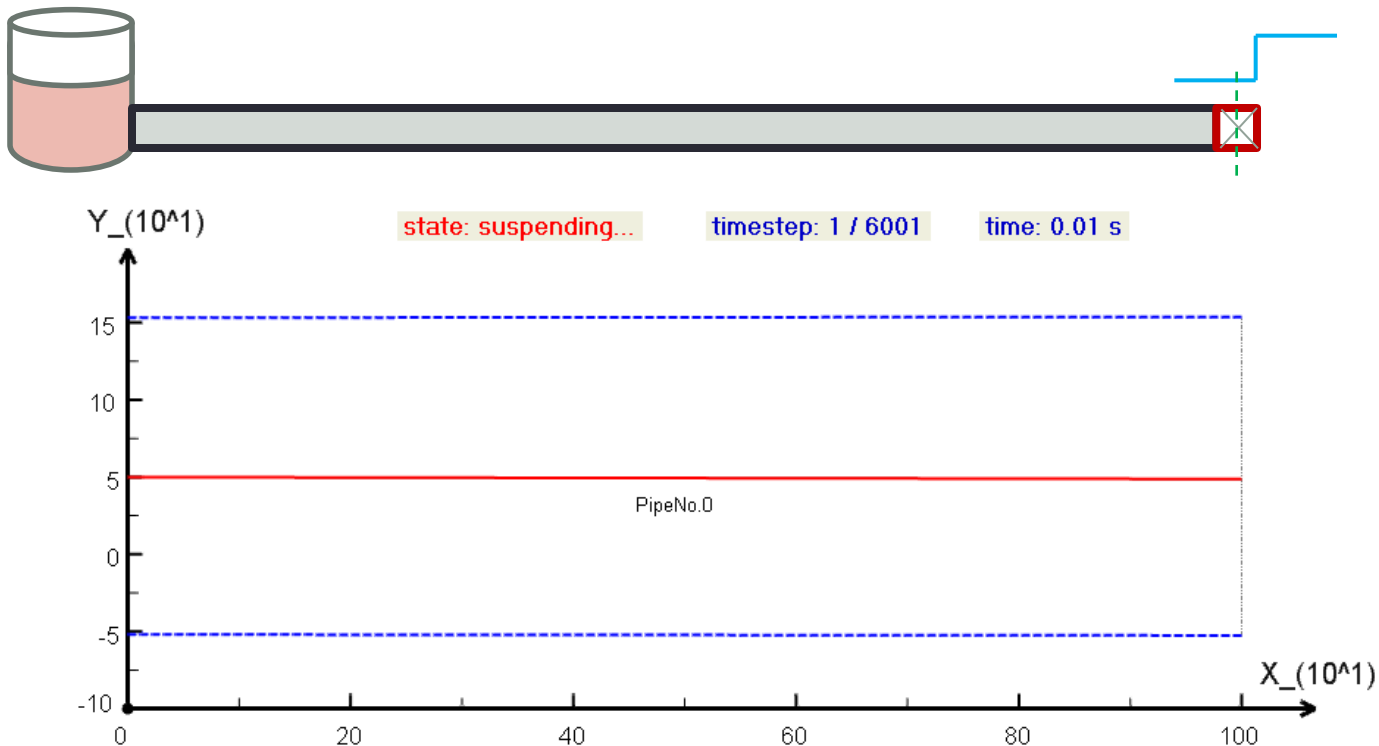
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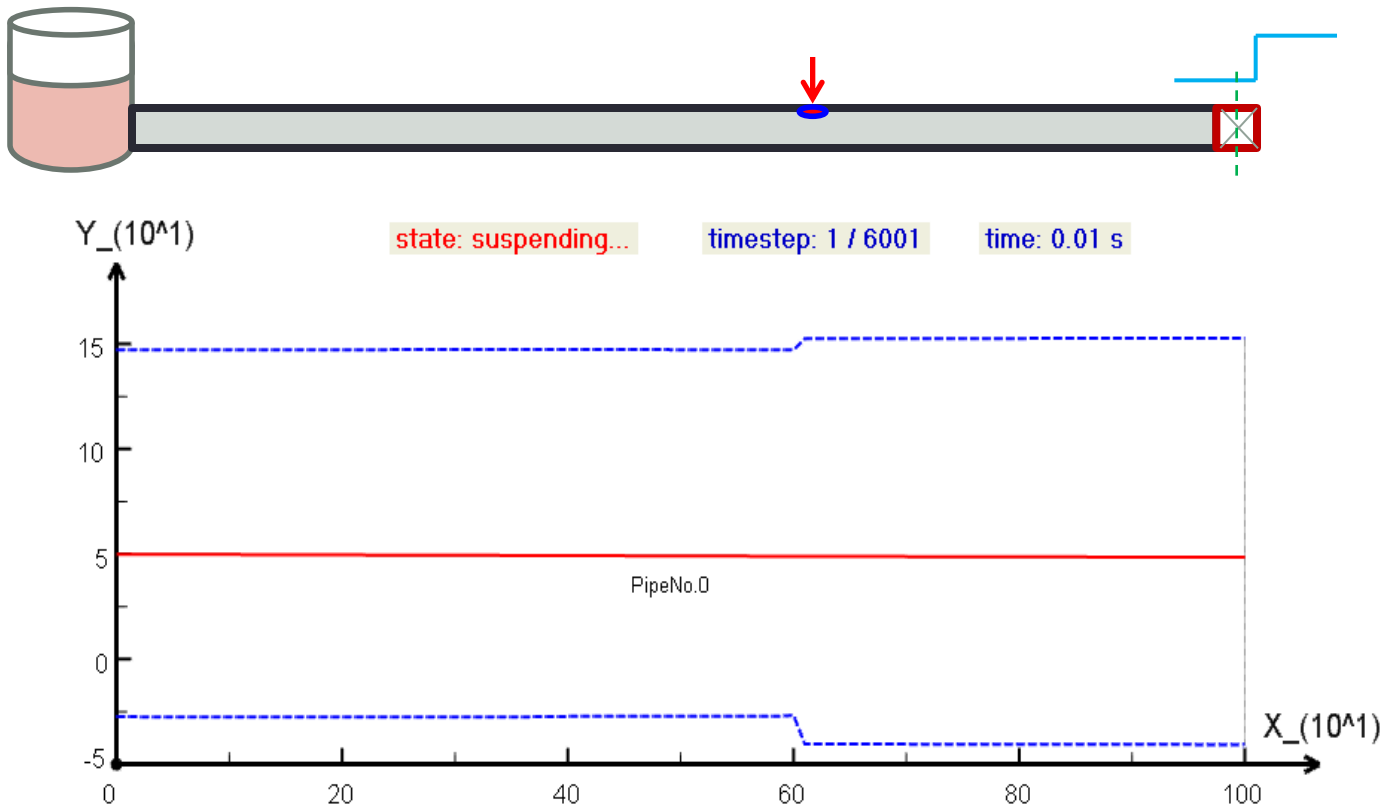
Transient Waves in Pressurized Pipelines

- Wave propagation in an “intact” pipeline system (defect-free)



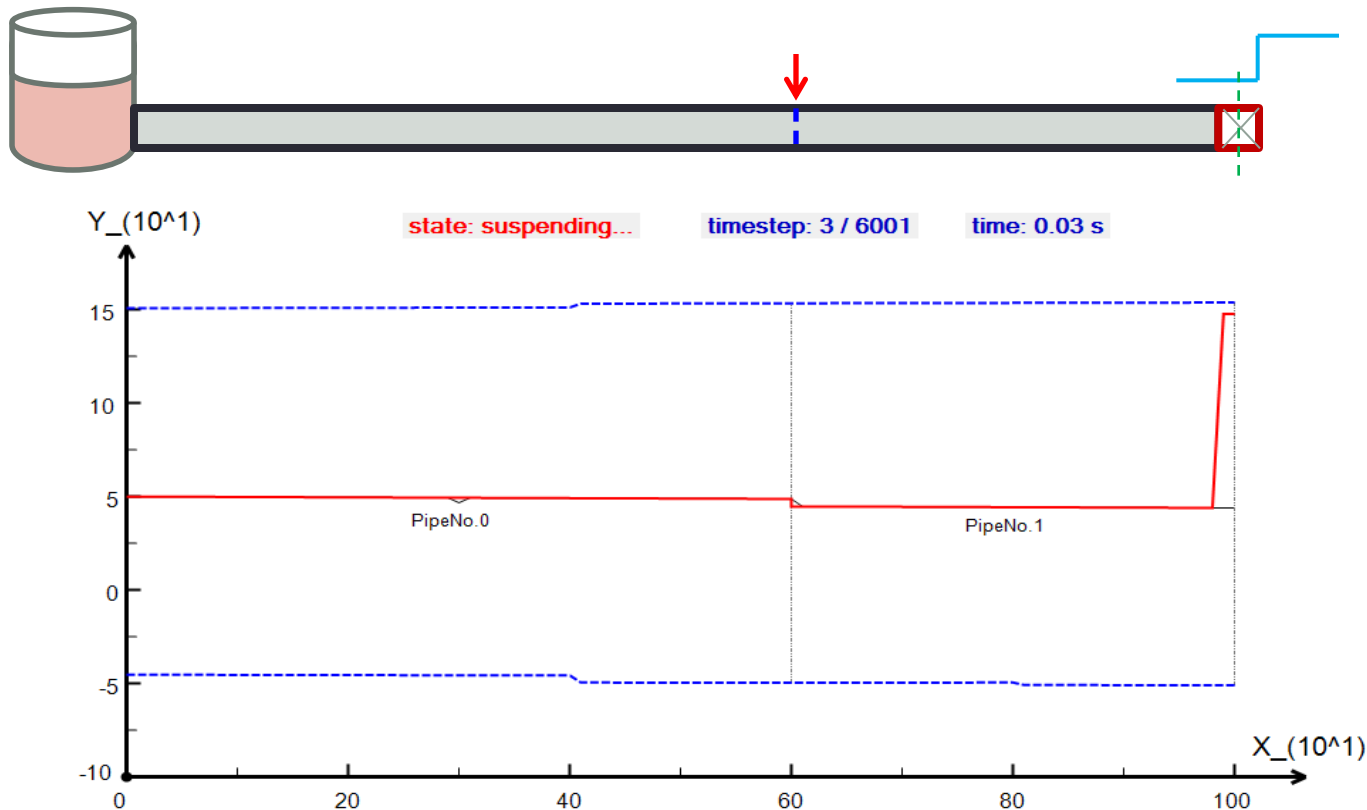
Transient Waves in Pressurized Pipelines

- Wave propagation in the pipeline with a **leakage** (e.g., crack/hole)



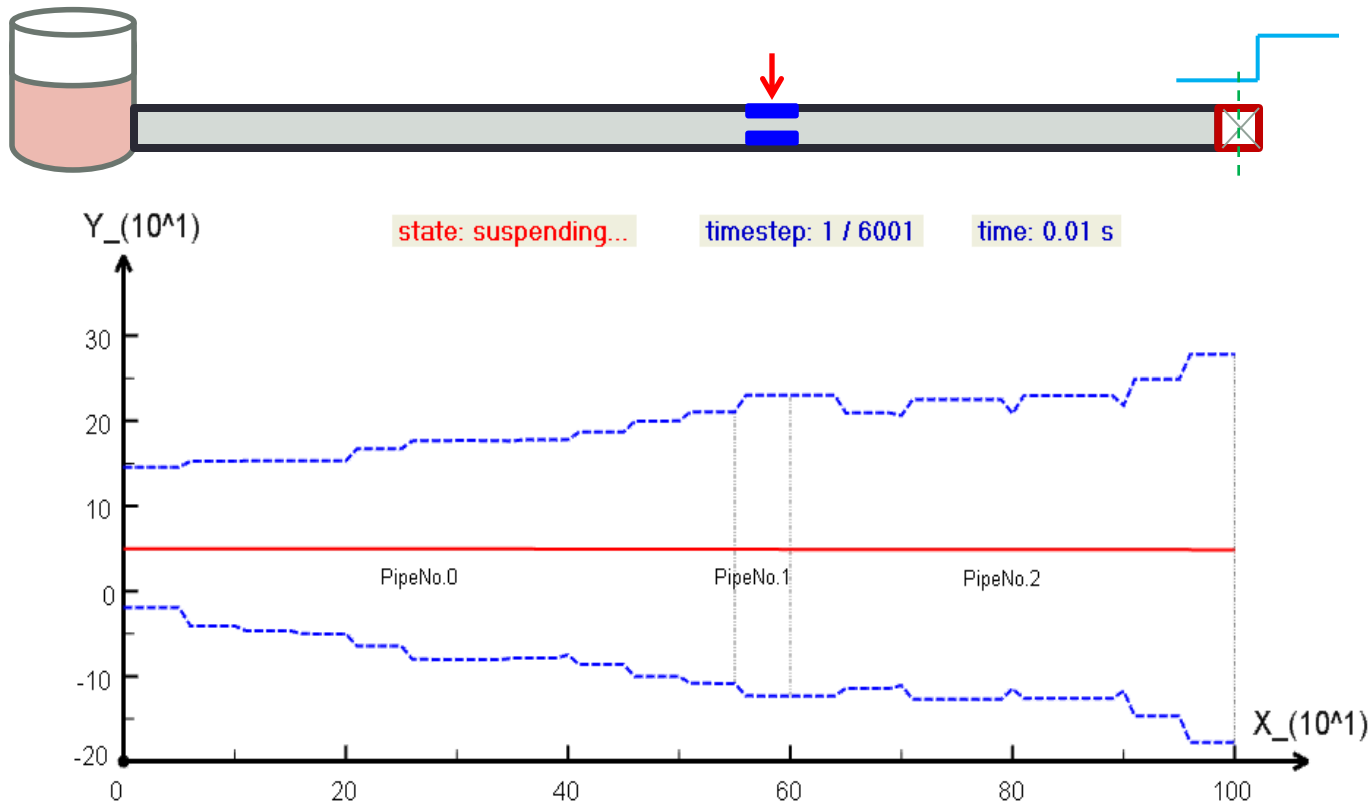
Transient Waves in Pressurized Pipelines

- Wave propagation in the pipeline with a **discrete blockage** (e.g., partially-closed inline valves)



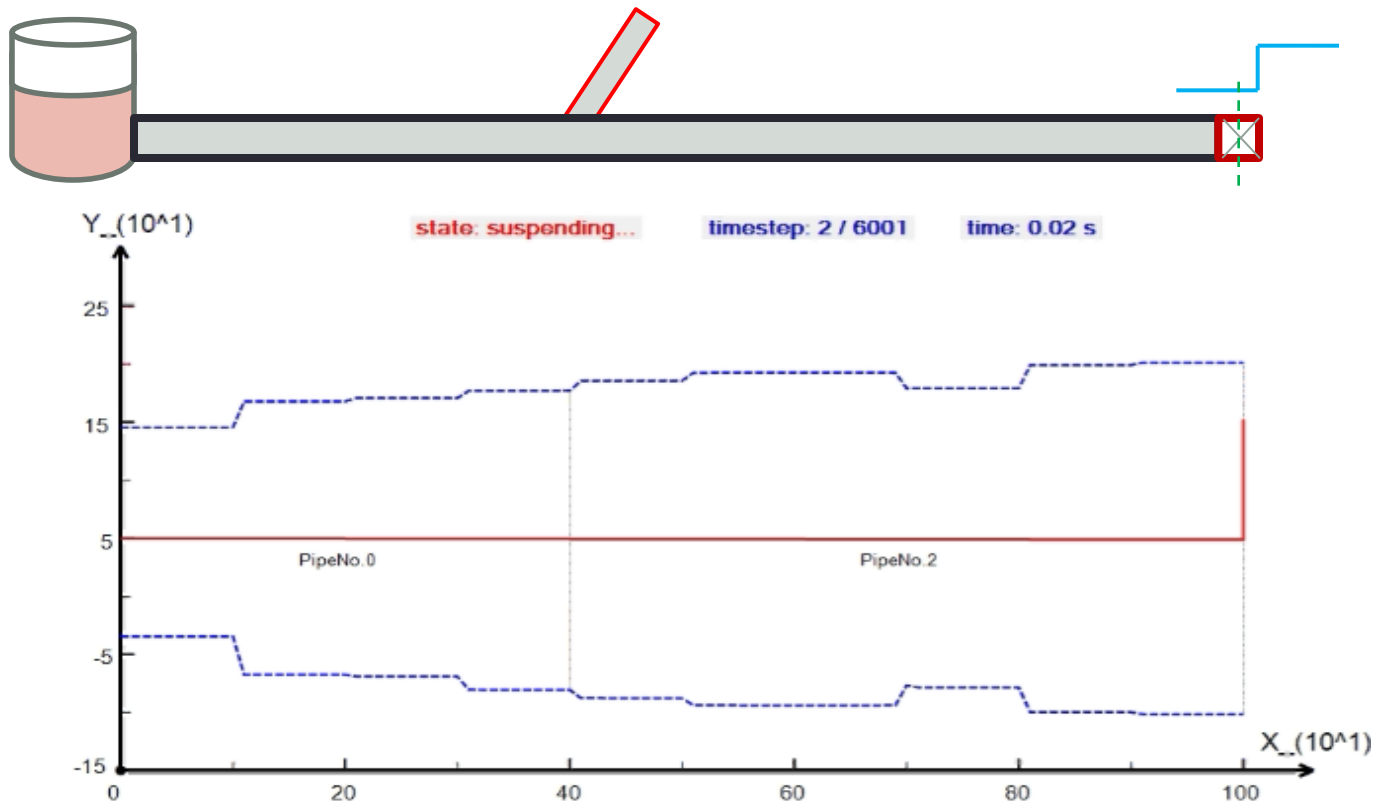
Transient Waves in Pressurized Pipelines

- Wave propagation in the pipeline with an **extended blockage** (e.g., corrosion/sediment)



Transient Waves in Pressurized Pipelines

- Wave propagation in the pipeline with a **dead-end side-branch** (e.g., illegal/unknown sections)



Information of Defects in Waves

- Reflections (oscillations)
 - Local inhomogeneities due to defects
 - Wave reflection / transmission / superposition
- Attenuation (damping)
 - Local head loss (turbulence/friction at defects)
 - Local mass loss (e.g., leaking/side-branch cases)

**Wave Reflections & Damping –
Essential Information for TBM**

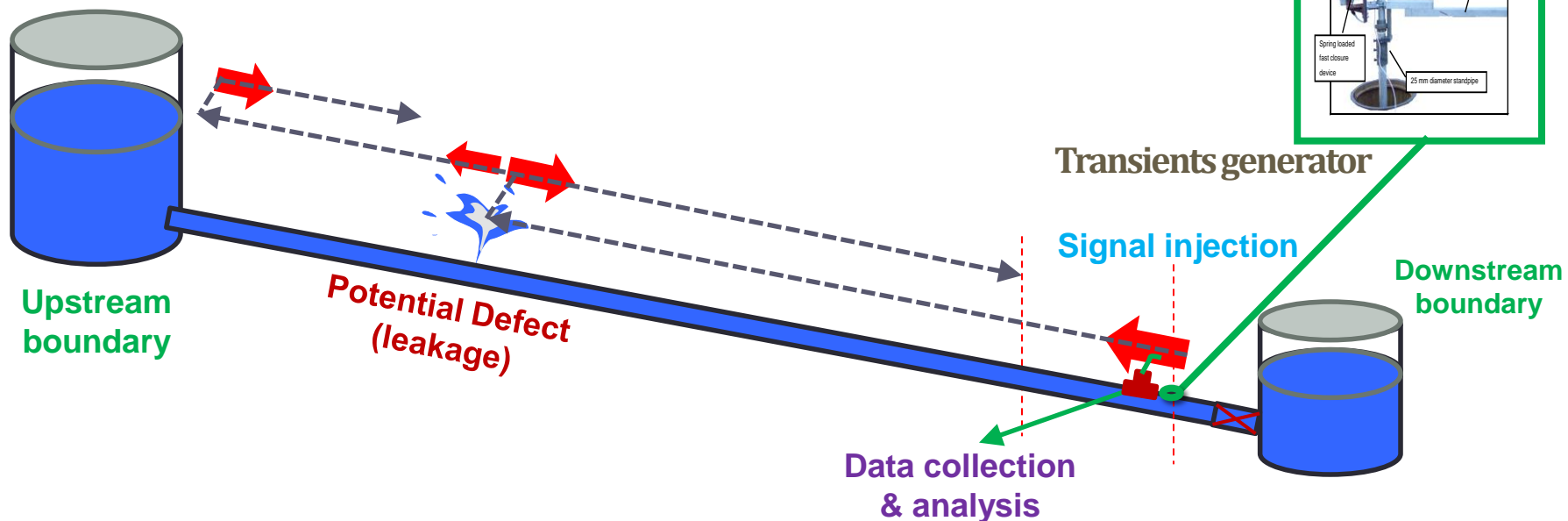
(Duan et al. 2010, etc.)

How to Utilize Wave Information in TBM?

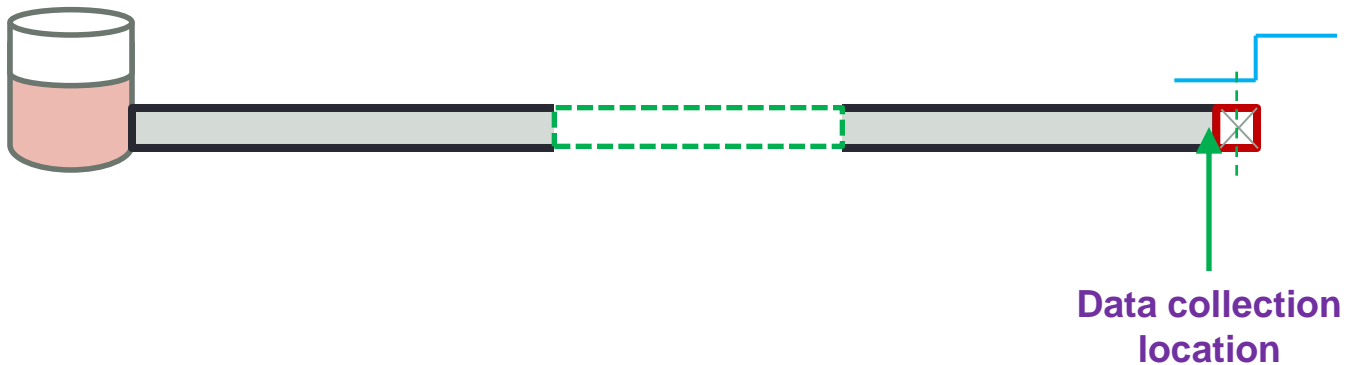
- Long-period wave methods (“whole” signal)
 - Direct calibration and analysis
 - Time-domain signal fitting
 - Frequency-domain signal fitting
 - Time consuming and data dependent
 - easily contaminated (turbulence, noises, low-flow stabilities)
- Short-period wave methods (partial signal):
 - Inverse analysis of analytical “pattern” (pre-derived)
 - Time-domain “pattern”
 - Frequency-domain “pattern”

Transient-Based Methods (TBM)

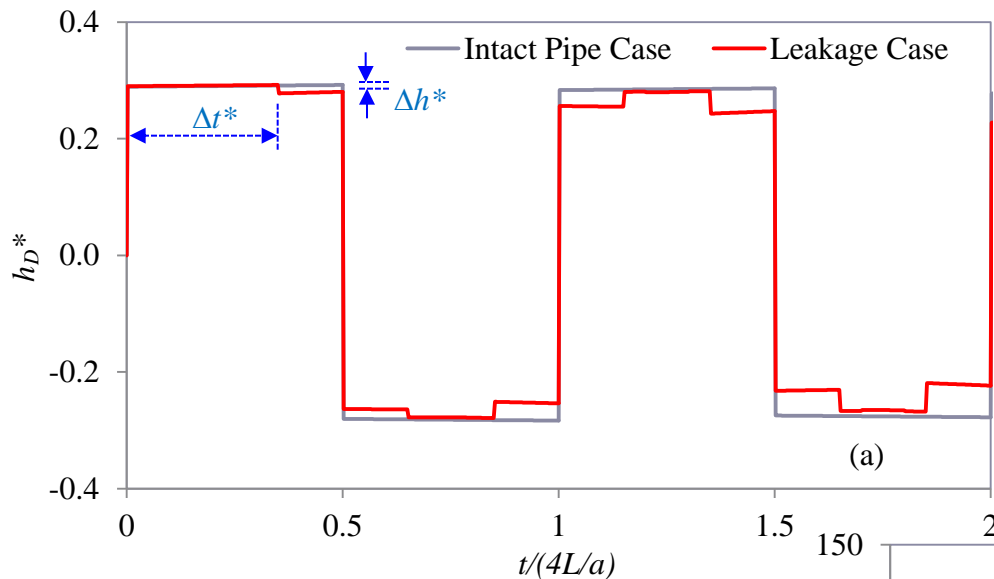
- Procedure of TBM for Defect Detection:
 - (a) Sending waves (input signals)
 - (b) Measuring signals at accessible locations (response signals)
 - (c) Analyzing data (characterizing noise/defects/system)
 - (d) Predicting defects (locating/sizing defects)



Part – 1: TBM for Single/Simple Pipe Systems



Transient Signature: Leakage



Time-domain:

$$x_L^* = 2\Delta t^*$$

$$A_L^* \approx \phi \Delta h^* (1 - \Delta h^*)^{-0.5}$$

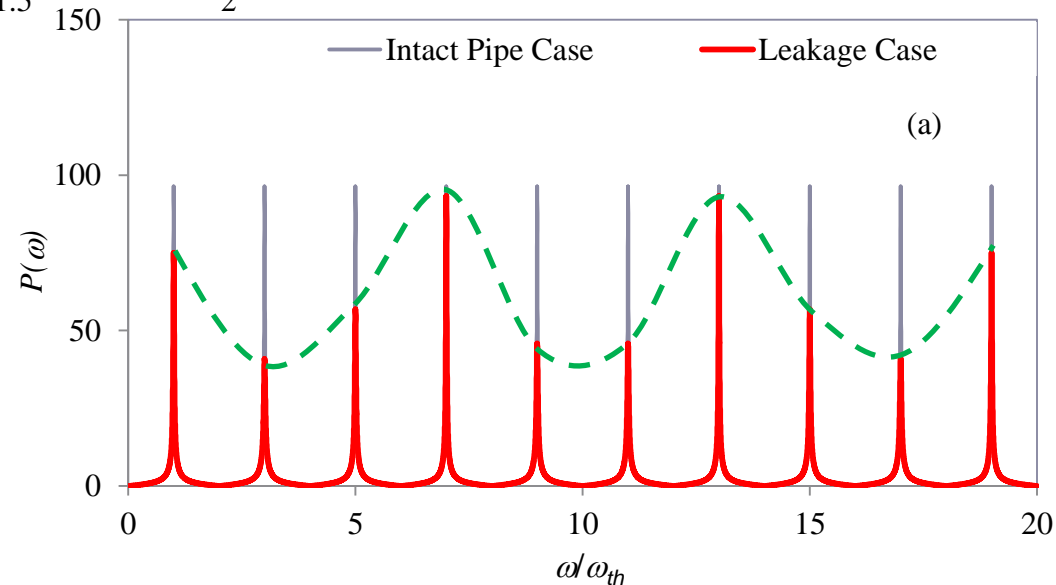
(Brunone 1999, etc.)

Frequency-domain:

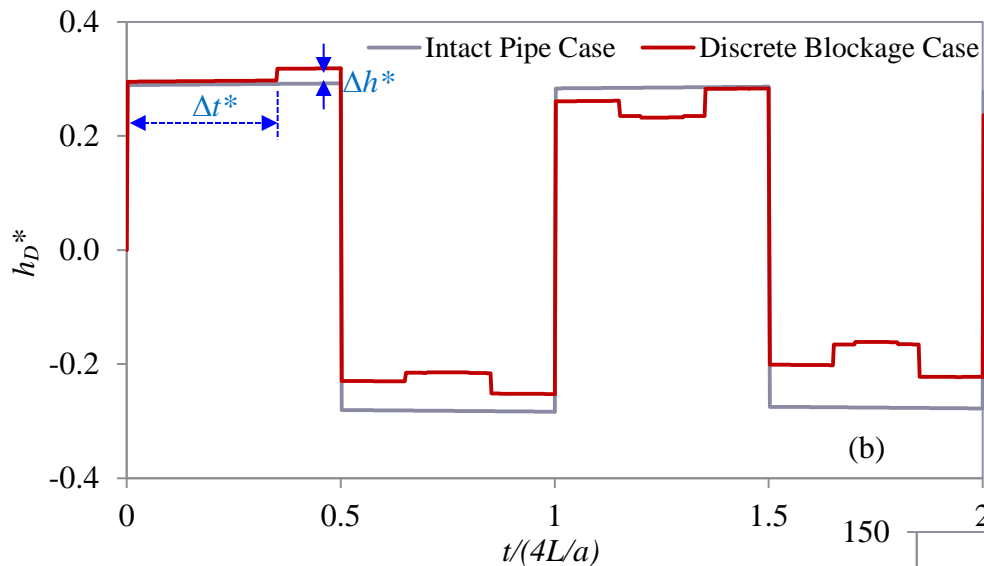
$$\hat{P} = \alpha \cos(2\pi k x_L^* - \theta) + \beta$$

x_L^* = leak location; α = leak size;
 k = number of resonant peaks;
 θ, β = coefficients

(Lee et al. 2006, etc.)



Transient Signature: Discrete Blockage



Time-domain:

$$x_L^* = 2\Delta t^*$$

$$\xi_{d0}^* \approx \Delta h^*$$

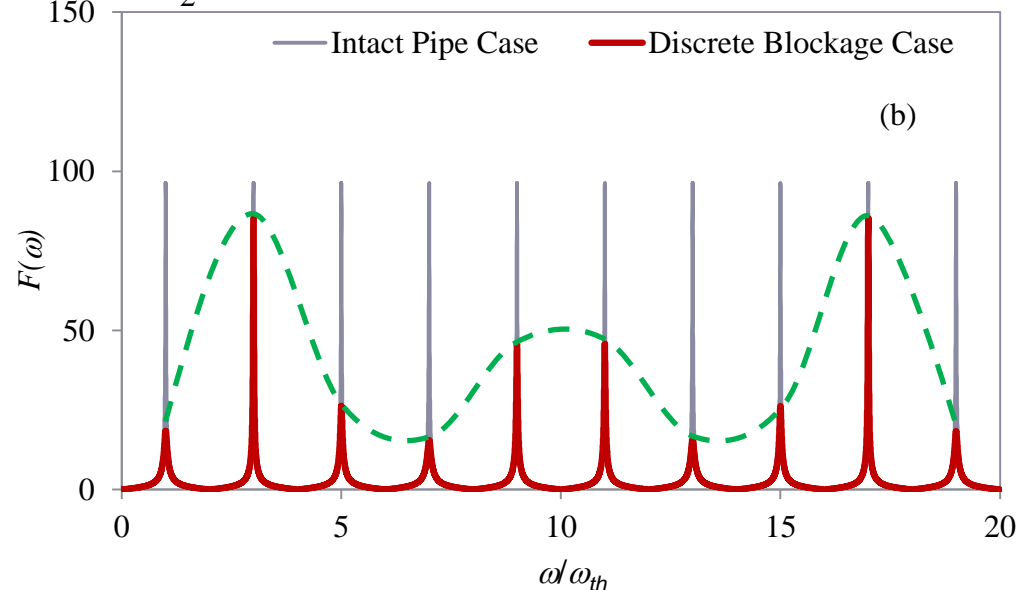
(Contractor 1965, Meniconi et al. 2011a, etc.)

Frequency-domain:

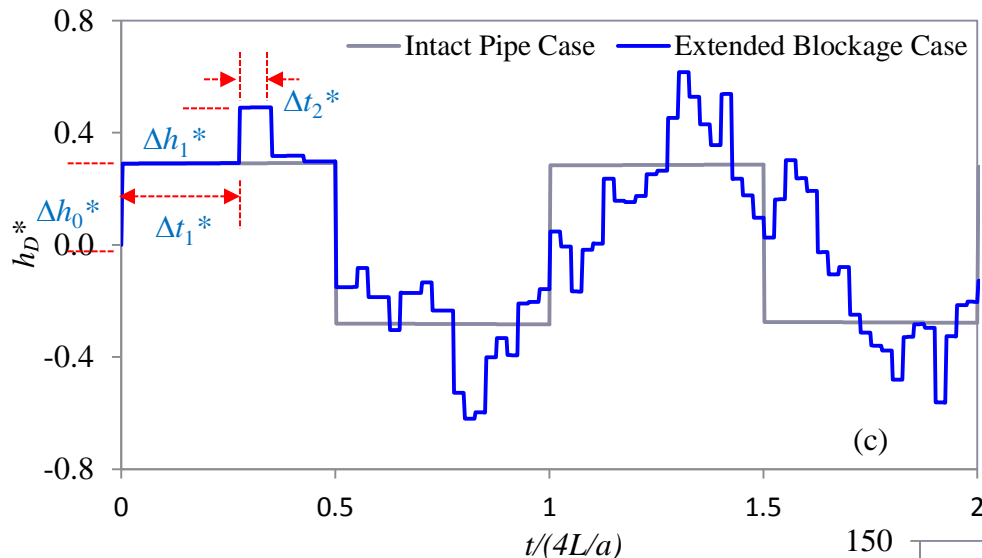
$$F^*(m) = I_B^* (1 + \cos(2\pi m x_B^* - \theta)) + \beta$$

x_B^* = discrete blockage location; I_B^* = discrete blockage impedance; m = number of resonant peaks; θ, β = coefficients

(Lee et al. 2008, etc.)



Transient Signature: Extended Blockage



Time-domain:

$$x_{bD}^* = 2\Delta t_1^*$$

$$L_b^* = 2\Delta t_2^*$$

$$A_b^* = \frac{A_b/a_b}{A_0/a_0} = \frac{\Delta h_0^* - \Delta h_1^*}{\Delta h_0^* + \Delta h_1^*}$$

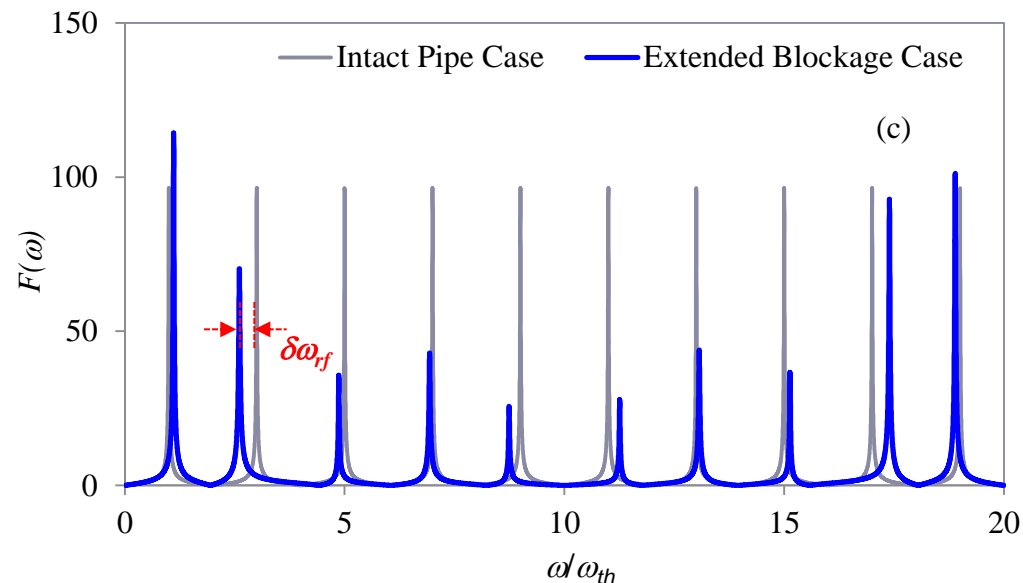
(Meniconi et al. 2013)

Frequency-domain:

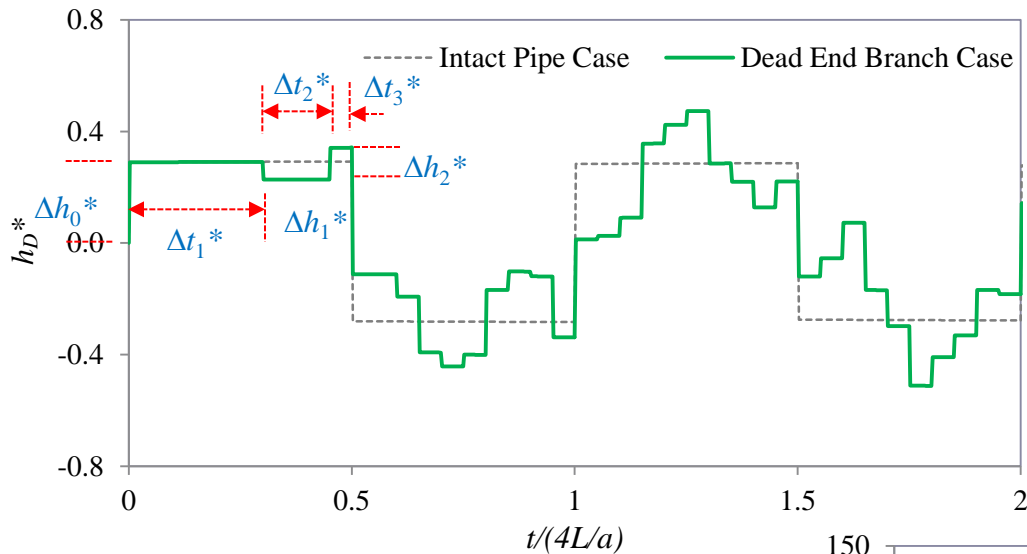
$$\delta\omega_{rf}^* \approx (-1)^{k+1} \frac{\varepsilon}{\pi} \sin[\lambda_2\omega_{rf0}] \sin[(\lambda_1 - \lambda_3)\omega_{rf0}]$$

$\delta\omega_{rf}^*$ = peak frequency shift; ω_{rf0} = system fundamental frequency; ε = relative blockage size; k = number of resonant peaks; $\lambda_i = L_i/a_i$ = wave propagation coefficients.

(Duan et al. 2012, 2013, etc.)



Transient Signature: Dead-End Side-Branch



Time-domain:

$$x_{SB}^* = 2\Delta t_1^*$$

$$L_{SB}^* = 2\Delta t_2^* \text{ or } 2|\Delta t_2^* \pm \Delta t_3^*|$$

$$A_{SB}^* = \frac{A_{SB}/a_b}{A_0/a_0} = f(\Delta h_0^*, \Delta h_1^*, \Delta h_2^*)$$

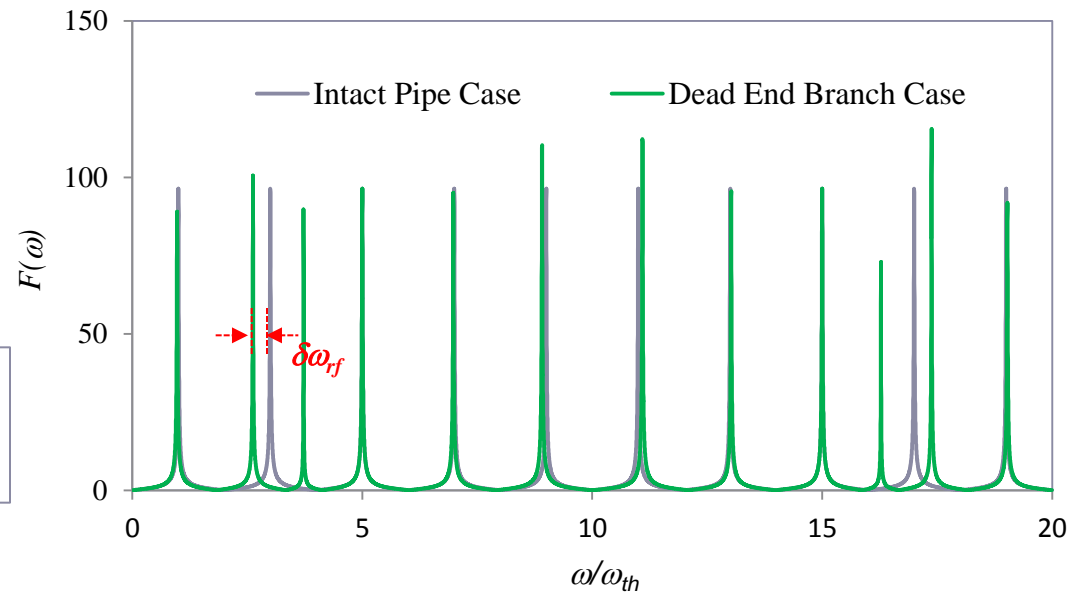
(Meniconi et al. 2011b)

Frequency-domain:

$$\delta\omega_{rf}^* = -\frac{2\varepsilon \sin[\lambda_3\omega_{rf0}] \cos^2[\lambda_2\omega_{rf0}]}{\pi \cos[\lambda_3\omega_{rf0}]}$$

$\delta\omega_{rf}^*$ = peak frequency shift; ω_{rf0} = system fundamental frequency; ε = relative branch size; $\lambda_i = L_i/a_i$ = propagation coefficients.

(Duan and Lee 2015)



Applications and Accuracy of TBM

- Numerical Applications (“Ideal” tests)
 - TDM:
 - Ferrante and Brunone (2003, 2004); Ferrante et al. (2007); Tuck et al. (2013, 2014);
 - Liggett and Chen (1994); Beck et al. (2005); AL-Khomairi (2008); etc.
 - FDM:
 - Lee et al. (2008, 2013, 2014); Duan et al. (2010, 2011, 2012a, 2012b, 2014, 2015);
 - Mpesha et al. (2001); Kim (2005); Mohapatra et al. (2006), Sattar et al. (2008); etc.
- Experimental Applications (Lab/Field tests)
 - TDM:
 - Brunone et al. (1999, 2001); Meniconi et al. (2009, 2011, 2012, 2013);
 - Stephens et al. (2004, 2008); Vitkovsky et al. (2007); etc.
 - FDM:
 - Lee et al. (2006, 2014); Duan et al. (2013, 2014); Meniconi et al. (2013);
 - Wang et al. (2002, 2005); Covas et al. (2005); etc.

Results: more accurate to locating defects than to sizing defects!

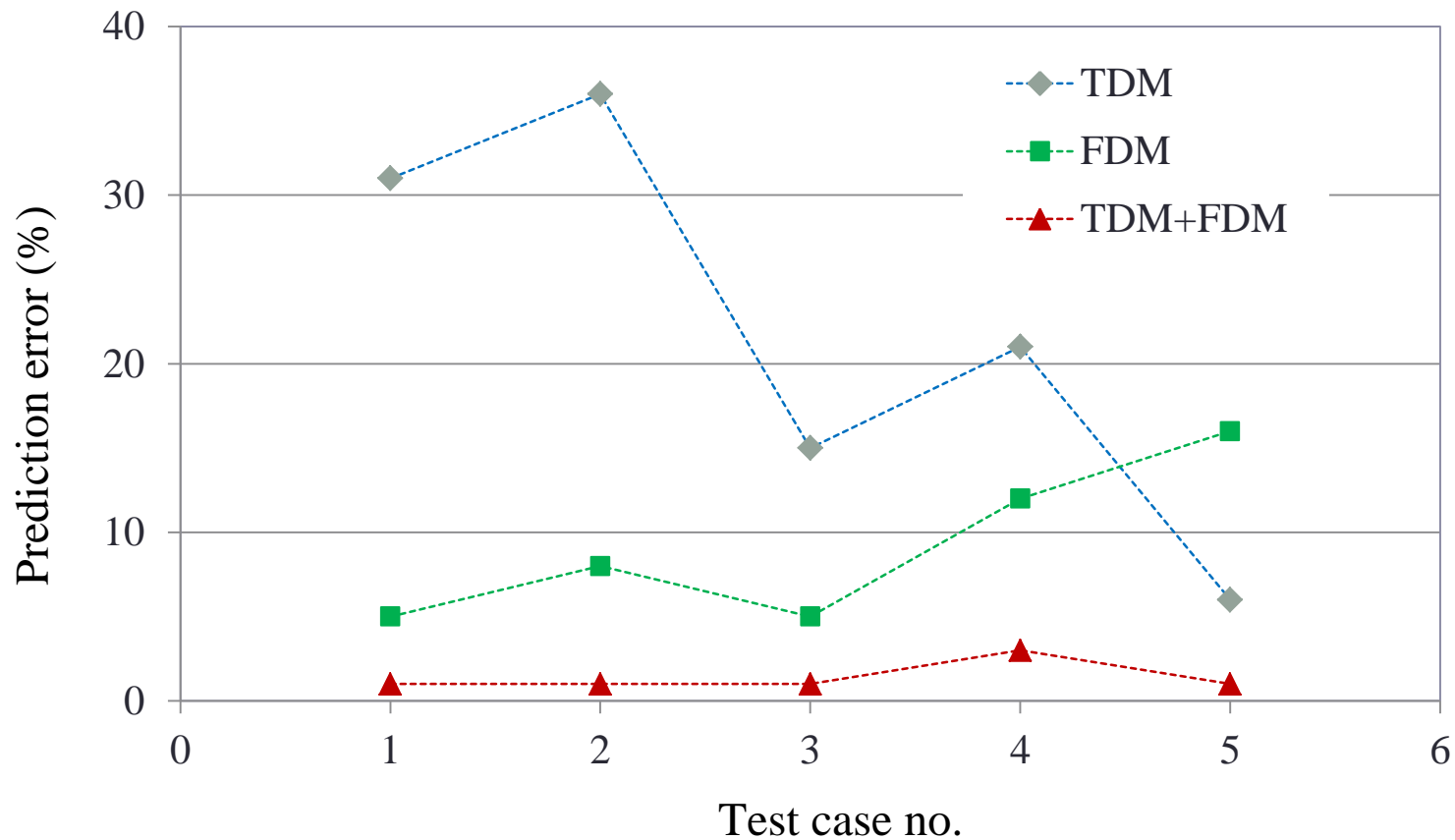
Comparison of TDM & FDM

(For simple pipe systems)

- Theoretically, both TDM & FDM are capable of detecting (locating and sizing) these four types of defects by the pre-derived “patterns”;
- **But in applications,**
 - FDM is more comprehensive and accurate than TDM, because some common complex factors such as friction and local dissipation effects are excluded in TDM;
 - TDM is more efficient and more simple to use than FDM in practical case studies.

Combination of TDM & FDM

- Meniconi et al. (2014) – Lab experiment tests
 - Pipe test system in New Zealand



Prediction for the length of extended blockage

Part – 2:
TBM for More Complex Pipe Systems
(Using FDM for Illustration)

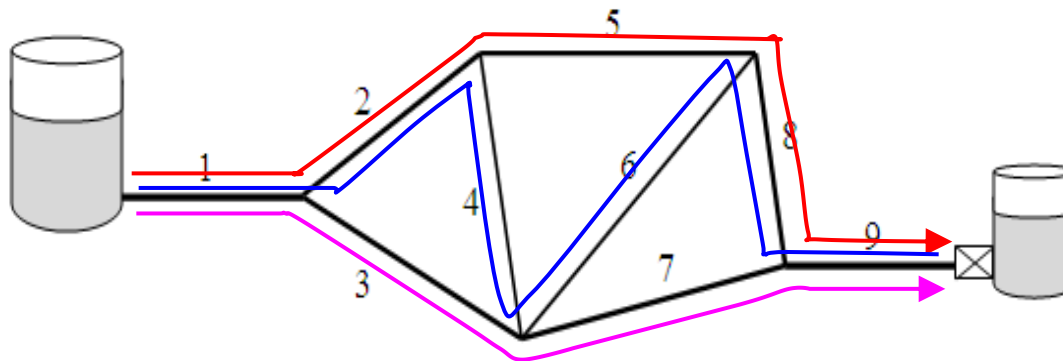
(2.1) Multiple-Pipe Systems

- Leakage in series pipes (Duan et al. 2011)

FDM – Pattern:
$$h_L^* = A_L^* \left[1 - \cos \left(2x_L^* \frac{\omega_{rf}}{a} L + \phi \right) \right]$$



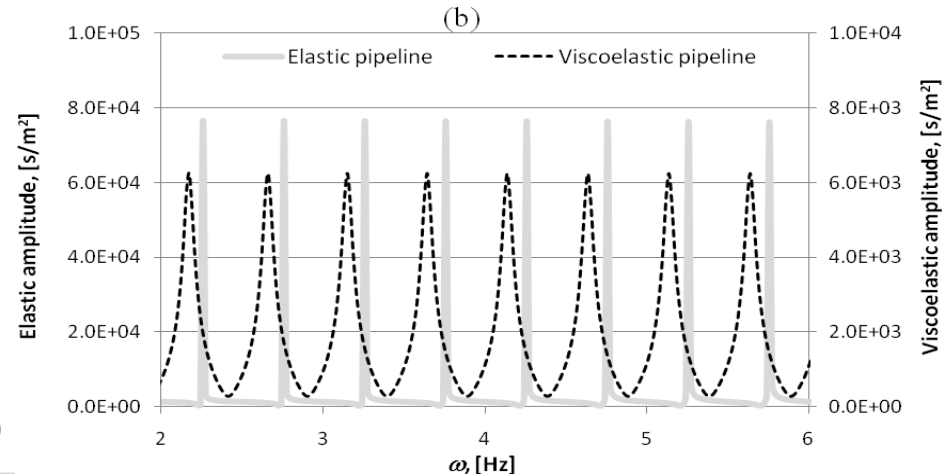
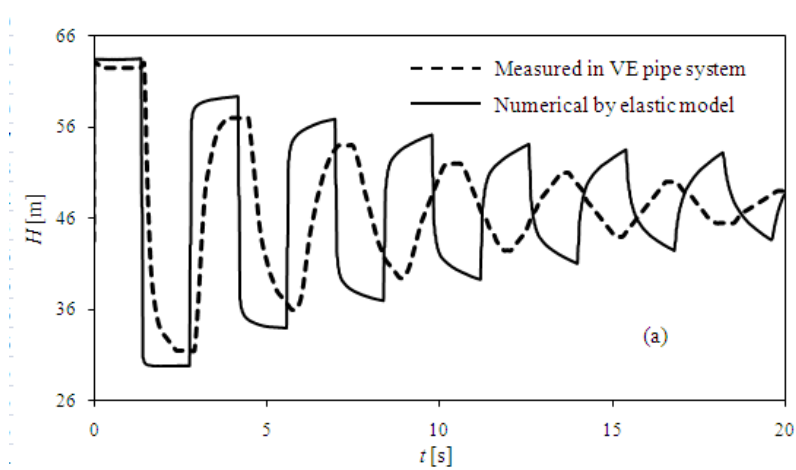
Leak information is independent of junctions



only 1/3 of original test work for this are needed!!!

(2.2) Viscoelastic Pipe Systems

- Plastic pipelines (Duan et al. 2012)



FDM – Pattern:

$$h_{leak-as}^* = A_{leak-as}^* \left(1 - \cos \left(2x_L^* \frac{\omega_{rf-VE}}{a} L \right) \right)$$

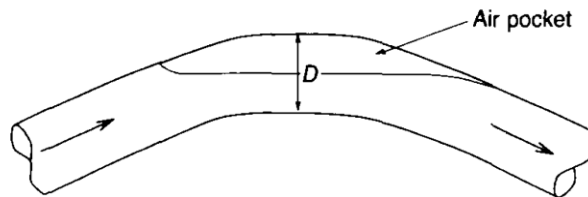
$$\omega_{rf-VE} = \frac{\omega_{rf-Elastic}}{\sqrt{W}}$$

W: visco-elastic parameter

The existing method can be extended to visco-elastic pipelines as long as the W is known!

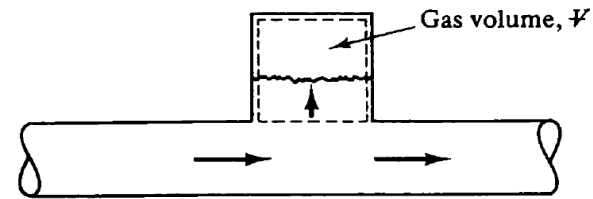
(2.3) Pipeline with Ends / Elbows

- Air-pocket detection (Duan & Lee &..., 2015)



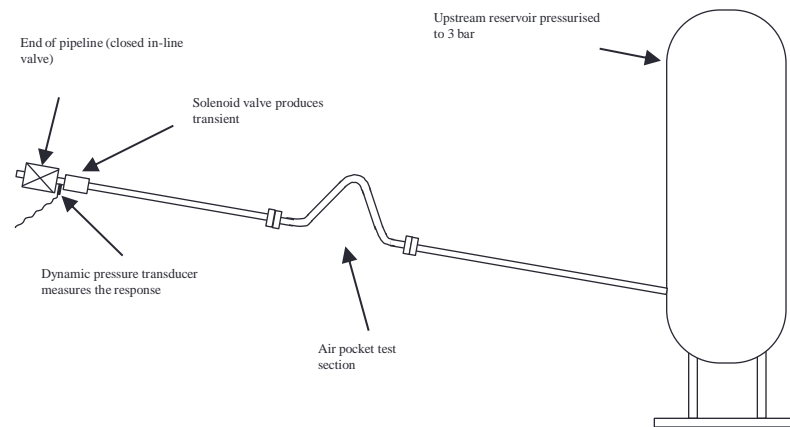
Inline air-pocket

(Burrows and Qiu 1995)



Offline air-pocket

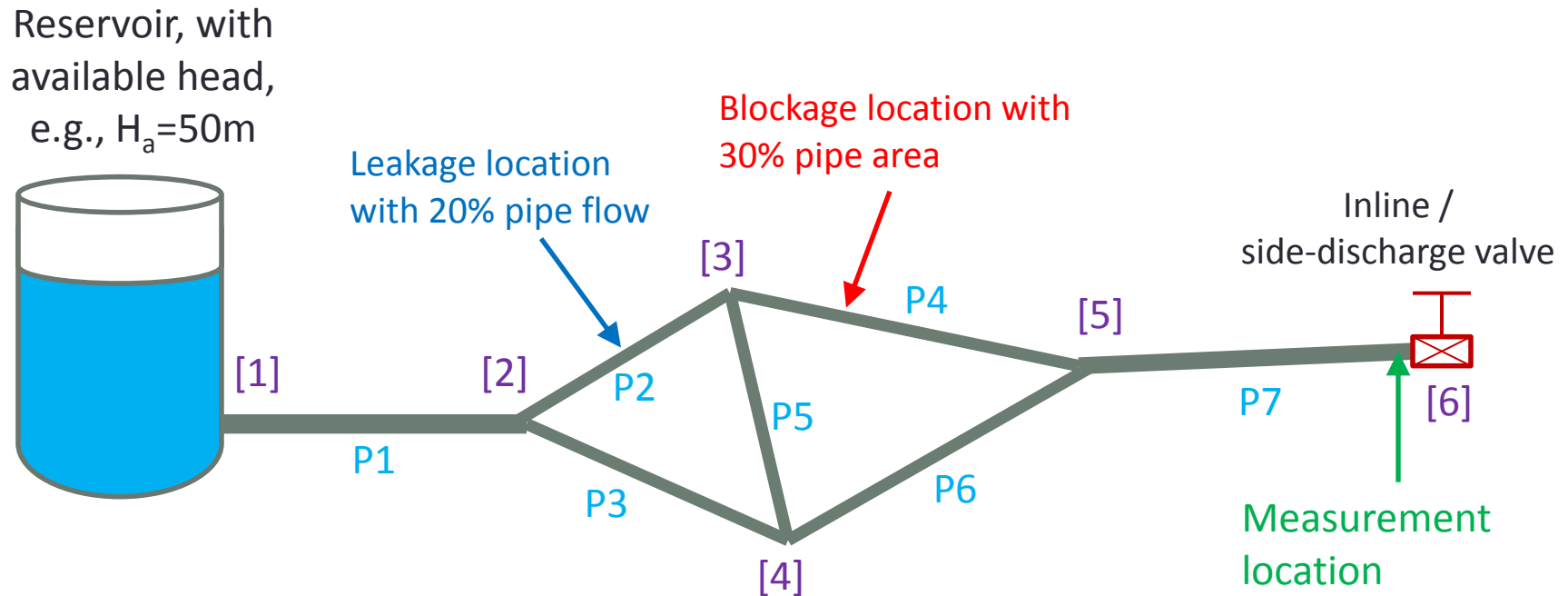
Streeter and Wylie (1993)



Experiment Test System (NZ)

(2.4) Pipe Networks

Numerical Test Case



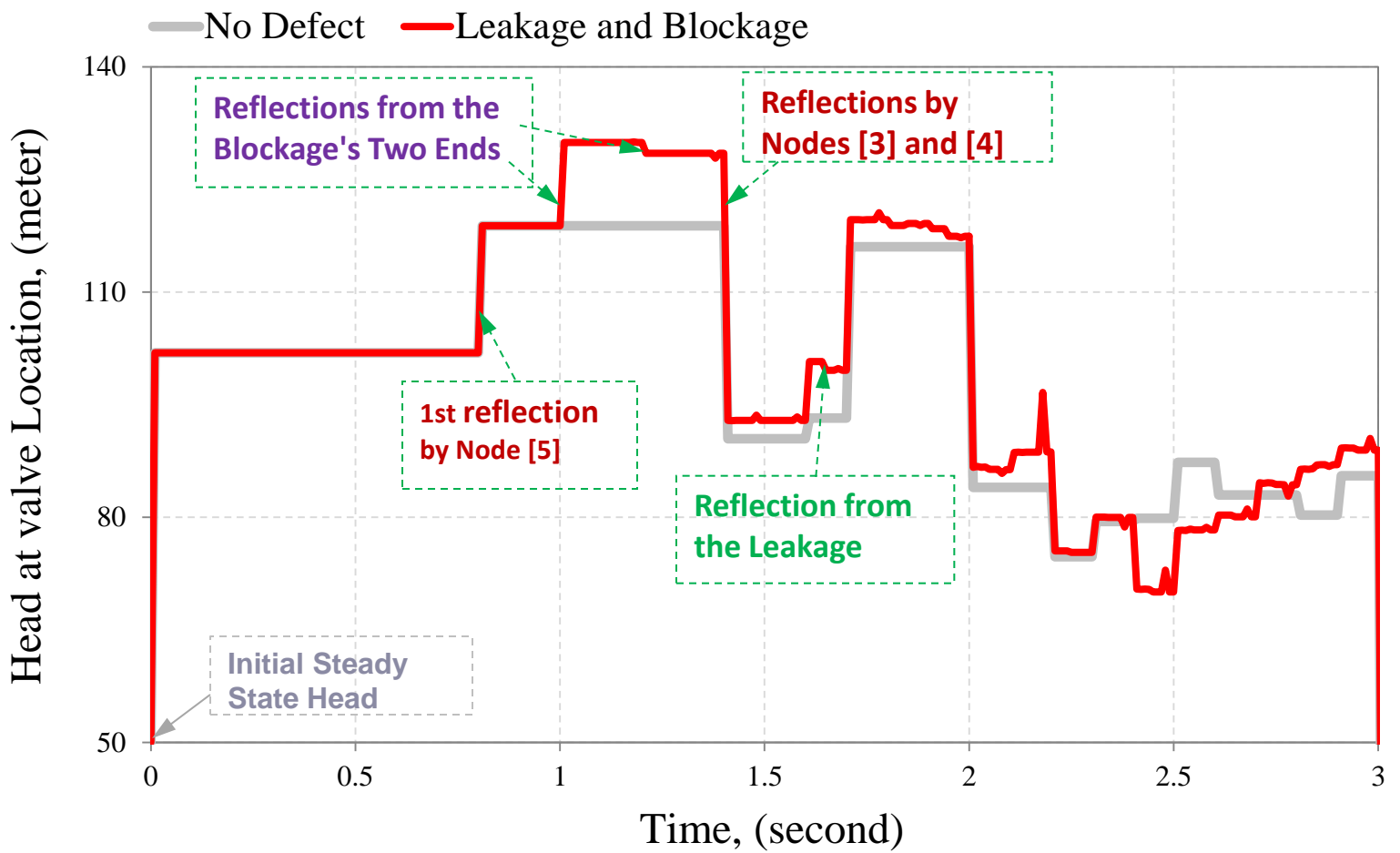
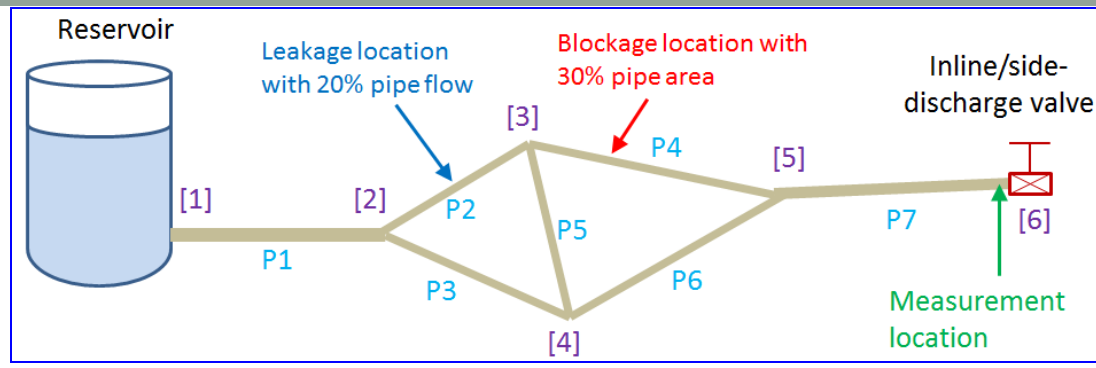
Notations:

[1] = nodal number

P1 = pipe number

Transient Responses at Valve

Numerical Results



Practical Influence Factors

- Input Signals (Lee et al. 2015)
 - Bandwidth
 - Amplitude
- System Complexities (Duan et al. 2011, 2015, etc.)
 - Pipe configurations
 - Defect characteristics (types, inhomogeneities)
 - Noises & uncertainties
 - ...

Future Development of TBM

(on the basis of current achievements)

- TDM & FDM (& Combination)
 - For complex pipe systems (e.g., networks)
 - Characterization of different types of defects
- LFW & HFW (& Combination)
 - Range vs. Resolution
 - Efficiency vs. Accuracy

Key References (by the Project Team Members)

- ❖ Brunone, B. (1999). A transient test-based technique for leak detection in outfall pipes. *J. of Water Resources Planning and Management*, ASCE, 125(5), 302-306.
- ❖ Duan, H.F., Lee, P.J., Ghidaoui, M.S., Tung, Y.K. (2010b). Essential system response information for transient-based leak detection methods. *J. of Hydraulic Research*, IAHR, 48(5), 650-657.
- ❖ Duan, H.F., Lee, P.J., Ghidaoui, M.S., and Tung, Y.K. (2011). Leak detection in complex series pipelines by using system frequency response method. *J. of Hydraulic Research*, IAHR, 49(2), 213-221.
- ❖ Duan H.F., Lee P.J., Ghidaoui M.S., Tung Y.K. (2012a). Extended blockage detection in pipelines by using the system frequency response analysis. *J. of Water Resources Planning and Management*, 138(1).
- ❖ Duan, H.F., Lee, P.J., Ghidaoui, M.S., and Tung, Y.K. (2012b). System response function based leak detection in viscoelastic pipeline. *J. of Hydraulic Engineering*, ASCE, 138(2), 143-153.
- ❖ Duan, H.F., Lee, P.J., Kashima, A., Lu, J.L., Ghidaoui, M.S., and Tung, Y.K. (2013). Extended blockage detection in pipes using the frequency response method: analytical analysis and experimental verification. *J. of Hydraulic Engineering*, ASCE, 139(7), 763-771.
- ❖ Lee, P.J., Lambert, M.F., Simpson, A.R., Vítkovský, J.P., Liggett J. (2006). Experimental verification of the frequency response method for pipeline leak detection. *J. of Hydraulic Research*, 44(5), 693-707.
- ❖ Lee, P.J., Vítkovský, J.P., Lambert, M.F., Simpson, A.R., Liggett J. (2008). Discrete blockage detection in pipelines using the frequency response diagram: numerical study. *J. of Hydraulic Engineering*, 134(5).
- ❖ Lee, P.J., Duan, H.F., Tuck, J., Ghidaoui, M. (2014). Numerical and experimental illustration of the effect of signal bandwidth on pipe condition assessment using fluid transients. *J. of Hydraulic Engineering*, 141(2).
- ❖ Meniconi, S., Brunone, B., and Ferrante, M. (2011a). In-line pipe device checking by short period analysis of transient tests. *J. of Hydraulic Engineering*, ASCE, 137(7), 713-722.
- ❖ Meniconi, S., Brunone, B., Ferrante, M., Massari, C. (2011b). Transient tests for locating and sizing illegal branches in pipe systems. *J. of Hydro-informatics*, 13(3), 334-345.
- ❖ Meniconi, S., Duan, H.F., Lee, P.J., Brunone, B., Ghidaoui, M.S., Ferrante, M. (2013). Experimental investigation of coupled frequency- and time-domain transient test-based techniques for partial blockage detection in pipelines. *J. of Hydraulic Engineering*, ASCE, 139(10), 1033-1040.
- ❖ etc.....

Thank you !